## DATA SHEET

## UAA3202M

Frequency Shift Keying (FSK) receiver

File under Integrated Circuits, IC01

## FEATURES

- Low cost single-chip FSK receiver
- Superheterodyne architecture with high integration level
- Few external low cost components
- Wide supply voltage range
- Low power consumption
- Wide frequency range, 150 to 450 MHz
- High sensitivity
- IF band determined by application
- High selectivity
- Very low spurious radiation, -60 dBm (meets FTZ 17TR2100)
- Automotive temperature range
- Power-down mode
- SSOP20 package.


## Applications

- Keyless entry systems
- Car alarm systems
- Remote control systems
- Security systems
- Telemetry systems
- Wireless data transmission
- Domestic appliances.


## GENERAL DESCRIPTION

The UAA3202M is a fully integrated single-chip receiver, primarily intended for use in VHF and UHF systems employing direct Frequency Shift Keying (FSK) modulation. The UAA3202M incorporates a SAW stabilized local oscillator, balanced mixer, IF amplifier, limiter, Received Signal Strength Indicator (RSSI), RSSI comparator, FSK demodulator, data filter and data slicer. The device features a power-down mode in order to minimize the average receiver supply current.

QUICK REFERENCE DATA

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {CC }}$ | supply voltage |  | 3.5 | - | 6 | V |
| ICC | supply current for operating mode on operating mode off | $\begin{aligned} & \mathrm{V}_{\mathrm{PWD}}=0 \mathrm{~V} ; \mathrm{R}_{2}=560 \Omega \\ & \mathrm{~V}_{\mathrm{PWD}}=\mathrm{V}_{\mathrm{CC}} \end{aligned}$ | $2.0$ | $\begin{array}{\|l\|} \hline 3.4 \\ 3 \end{array}$ | $\begin{aligned} & 4.7 \\ & 30 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mu \mathrm{~A} \end{aligned}$ |
| $\mathrm{P}_{\text {sens }}$ | sensitivity | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{i}}=433.92 \mathrm{MHz} ; \\ & \mathrm{f}_{\text {mod }}=250 \mathrm{~Hz} \text { square wave; } \\ & \Delta \mathrm{f}= \pm 25 \mathrm{kHz} ; \mathrm{BER} \leq 3 \% \\ & \hline \end{aligned}$ | - | - | -94 | dBm |
| $\mathrm{T}_{\text {amb }}$ | operating ambient temperature |  | -40 | - | +85 | ${ }^{\circ} \mathrm{C}$ |

ORDERING INFORMATION

| TYPE <br> NUMBER | PACKAGE |  |  |
| :---: | :---: | :---: | :---: |
|  | NAME | DESCRIPTION | VERSION |
| UAA3202M | SSOP20 | plastic shrink small outline package; 20 leads; body width 5.3 mm | SOT339-1 |

Frequency Shift Keying (FSK) receiver

## BLOCK DIAGRAM



Fig. 1 Block diagram.

Frequency Shift Keying (FSK) receiver

PINNING

| SYMBOL | PIN | DESCRIPTION |
| :--- | :---: | :--- |
| MON | 1 | negative mixer output |
| MOP | 2 | positive mixer output |
| V $_{\text {CC }}$ | 3 | positive supply voltage |
| OSC | 4 | oscillator collector |
| OSE | 5 | oscillator emitter |
| V $_{\text {EO }}$ | 6 | negative supply voltage for oscillator |
| V $_{\text {EE }}$ | 7 | negative supply voltage |
| COMP | 8 | RSSI comparator output |
| CPB | 9 | comparator input B |
| CPA | 10 | comparator input A |
| DATA | 11 | data output |
| PWD | 12 | power-down control input |
| CPC | 13 | comparator input C |
| DMOD | 14 | demodulator frequency adjustment |
| RSSI | 15 | RSSI current output |
| LFB | 16 | limiter feedback |
| LIN | 17 | limiter input |
| MXIN | 18 | mixer input |
| $V_{\text {EM }}$ | 19 | negative supply voltage for mixer |
| FA | 20 | IF amplifier output |



Fig. 2 Pin configuration.

## FUNCTIONAL DESCRIPTION

The device is based on the superheterodyne architecture incorporating a mixer, local oscillator, IF amplifier, limiter, RSSI, RSSI comparator, FSK demodulator, data filter, data slicer and power-down circuitry. The device employs a low IF frequency of typically 1 MHz in order to allow IF filtering by means of external low cost $R, L$ and $C$ components. If image rejection is required it can be achieved by applying a matching external front-end SAW filter. The device provides a wide IF range of 300 kHz in order to allow the use of a SAW stabilized oscillator.

The on-chip local oscillator provides the injection signal for the mixer. Tuning of the on-chip local oscillator is not necessary. The oscillator frequency is determined by an external 1-port SAW resonator. The RF input signal is fed to the mixer and down converted to the IF frequency. After amplification and filtering the RF signal is applied to a limiter. The IF filter order and characteristics are determined by the external low cost $R, L$ and $C$ components. The limiter amplifier provides a RSSI signal which can be routed to an on-chip RSSI level comparator in order to derive a field strength indication for external use. The limited IF signal is fed to the FSK demodulator. The demodulator centre frequency is determined by an external capacitor. No alignment is necessary for the FSK demodulator. After filtering the demodulated data signal is fed to a data slicer and is made available at the data output. The data filter characteristics are determined by external capacitors. The data slicer employs an adaptive slice reference in order to track frequency offsets.

The device is switched from power-down to operating mode and vice versa by means of a control input. Extremely low supply current is drawn when the device is in power-down mode. Measures are taken to allow fast receiver settling when the device is switched from power-down to operating mode.

## Mixer

The mixer is a single balanced emitter coupled mixer with internal biasing. Matching of the RF source impedance to the mixer input requires an external matching network.

## Oscillator

The oscillator consists of an on-chip transistor in common base configuration. An external tank and SAW resonator determines the oscillator frequency. Oscillator alignment is not necessary. Oscillator bias is controlled by an external resistor.

## Post mixer amplifier

The Post Mixer Amplifier (PMA) is a differential input, single-ended output amplifier. It separates the first and second IF filters from each other. Amplifier gain is provided in order to reduce the influence of the limiter noise figure on the total noise figure.

## Limiter

The limiter is a single-ended input multiple stage amplifier with high total gain. Amplifier stability is achieved by means of an external DC feedback capacitor, which is also used to determine the lower limiter cut-off frequency. An RSSI signal proportional to the limiter input signal is provided.

## IF filters

IF filtering with high selectivity is realized by means of external low cost R, L and C components. The first IF filter is located directly following the mixer output. An external L/C network assembles a band-pass with low sensitivity in order to meet the bandwidth of an elliptic low-pass filter external to the device and is located in front of the limiter. The filter source impedance is determined by the drive impedance of the IF amplifier. In order to improve the IF filter selectivity below the pass-band a high-pass characteristic is added by means of a DC blocking capacitor in front of the limiter input and by means of the limiter DC feedback capacitor.

## RSSI

The RSSI signal is a current proportional to the limiter input level (RF input power). By means of an external resistor the resulting RSSI voltage level is set in order to fit the application. The RSSI voltage is available to external circuits and is fed to the input of the RSSI level comparator. For RSSI filtering an external capacitor is connected.

## RSSI level comparator

The RSSI level comparator compares the RSSI level with a fixed and independent internal reference voltage. If the RSSI level exceeds the internal reference voltage a logic HIGH signal is generated. The level comparator provides some hysteresis in order to avoid spurious oscillation. The output of the level comparator is designed as an open-collector with internal pull-up.

## FSK demodulator

The limited IF signal is converted into baseband data by means of a quadrature FM demodulator consisting of an all-pass filter and a mixer stage. No alignment of the demodulator is necessary. The demodulator centre frequency is set by a capacitor external to the device. The demodulator provides a large audio bandwidth in order to allow high data rate applications.
The demodulator can detect a small IF frequency deviation even if a relatively large IF frequency offset is encountered.

## Data filters

After demodulation a two-stage data filtering circuit is provided in order to suppress unwanted frequency components. Two R/C low-pass filters with on-chip resistors are provided which are separated by a buffer stage.

## Data slicer

Data detection is provided by means of a level comparator with adaptive slice reference. After the first data filter stage the pre-filtered data is split into two parts. One part passes the second data filter stage and is fed to the positive comparator input.

The other path is fed to an integration circuit with a large time constant in order to derive the average value (DC component) as an adaptive slice reference which is presented to the negative comparator input. The adaptive reference enables the received data over a large range of demodulator frequency offsets to be detected.
The integration circuit consists of a simple R/C low-pass filter with on-chip resistor. The level comparator output is designed as an open-collector with internal pull-up.

## Power-down circuitry

The device provides a power-down mode. While in power-down mode the device disables the majority of the internal circuits and consumes extremely low current. Measures are taken to allow fast receiver settling when normal operation is resumed. Thus circuits with large time constants are only powered down partly or provide a high impedance during power-down in order to avoid the discharge of external capacitors as much as possible. Power-down mode is entered when the control input is active HIGH. The control input provides an internal pull-up resistor of high impedance.

## LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 134).

| SYMBOL | PARAMETER | CONDITIONS | MIN. | MAX. | UNIT |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{V}_{\text {CC }}$ | supply voltage |  | -0.3 | +8.0 | V |
| $\mathrm{~T}_{\text {amb }}$ | operating ambient temperature |  | -40 | +85 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {stg }}$ | storage temperature |  | -55 | +125 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {esd }}$ | electrostatic handling |  |  |  |  |
|  | pins 4 and 5 |  |  |  |  |
|  | pins 18 and 19 |  |  |  |  |
|  | all other pins |  | -2000 | +1500 | V |
|  |  | -1500 | +2000 | V |  |

## Note

1. Human body model: equivalent to discharging a 100 pF capacitor through a $1.5 \mathrm{k} \Omega$ series resistor.

THERMAL CHARACTERISTICS

| SYMBOL | PARAMETER | VALUE | UNIT |
| :--- | :--- | :---: | :---: |
| $\mathrm{R}_{\text {th } \mathrm{j}-\mathrm{a}}$ | thermal resistance from junction to ambient in free air | 125 | K/W |

## DC CHARACTERISTICS

$\mathrm{V}_{\mathrm{CC}}=3.5 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; for application diagram see Fig. 11 ; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supplies |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{CC}}$ | supply voltage |  | 3.5 | - | 6 | V |
| $\mathrm{I}_{\mathrm{CC}}$ | supply current for operating mode on operating mode off | note 1 $\begin{aligned} & \mathrm{V}_{\mathrm{PWD}}=0 \mathrm{~V} ; \\ & \mathrm{R}_{2}=560 \Omega \\ & \mathrm{~V}_{\mathrm{PWD}}=\mathrm{V}_{\mathrm{CC}} \end{aligned}$ | 2.0 - | 3.4 <br> 3 | $\begin{aligned} & 4.7 \\ & 30 \end{aligned}$ | mA <br> $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {PWD(0n) }}$ | PWD voltage for operating mode ON |  | 0 | - | 300 | mV |
| $\mathrm{V}_{\text {PWD(off) }}$ | PWD voltage for operating mode OFF |  | $\mathrm{V}_{\mathrm{CC}}-0.3$ | - | $\mathrm{V}_{\mathrm{CC}}$ | V |
| IPWD(on) | PWD current for operating mode ON | $\mathrm{V}_{\text {PWD }}=0 \mathrm{~V}$ | -30 | -10 | -3 | $\mu \mathrm{A}$ |
| IPWD(off) | PWD current for operating mode OFF | $\mathrm{V}_{\mathrm{PWD}}=\mathrm{V}_{\mathrm{CC}}$ | - | 1 | 3 | $\mu \mathrm{A}$ |
| Oscillator |  |  |  |  |  |  |
| V OSC (DC) | DC operating point pin 4 |  | 3.28 | 3.34 | 3.40 | V |
| Mixer |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{MXIN}(\mathrm{DC})}$ | DC operating point pin 18 |  | 0.68 | 0.78 | 0.88 | V |
| $\mathrm{V}_{\text {MOP(DC) }}$ | DC operating point pin 2 |  | 2.78 | 2.98 | 3.18 | V |
| $\mathrm{V}_{\text {MON(DC) }}$ | DC operating point pin 1 |  | 2.78 | 2.98 | 3.18 | V |
| Post mixer amplifier |  |  |  |  |  |  |
| $\mathrm{V}_{\text {FA(DC) }}$ | DC operating point pin 20 |  | 2.14 | 2.27 | 2.40 | V |
| Limiter |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{LIN}(\mathrm{DC})}$ | DC operating point pin 17 |  | 3.45 | 3.49 | 3.50 | V |
| $\mathrm{V}_{\text {LFB(DC) }}$ | DC operating point pin 16 |  | 2.76 | 2.81 | 2.86 | V |
| $\left.\mathrm{V}_{\text {RSSII }} \mathrm{DC}\right)$ | DC operating point pin 15 |  | 2.21 | 2.36 | 2.51 | V |
| Demodulator |  |  |  |  |  |  |
| V ${ }_{\text {DMOD(DC) }}$ | DC operating point pin 14 |  | 1.63 | 1.83 | 2.03 | V |
| Data slicer |  |  |  |  |  |  |
| $\mathrm{V}_{\text {CPC(DC) }}$ | DC operating point pin 13 | note 2 | 1.43 | 1.93 | 2.43 | V |
| $\mathrm{V}_{\text {CPA(DC) }}$ | DC operating point pin 10 | note 2 | 1.43 | 1.93 | 2.43 | V |
| $\mathrm{V}_{\text {CPB(DC) }}$ | DC operating point pin 9 | note 2 | 1.43 | 1.93 | 2.43 | V |
| $\mathrm{V}_{\text {OH( }{ }^{\text {DAT }} \text { ) }}$ | HIGH-level data output voltage | $\mathrm{I}_{\text {DATA }}=-10 \mu \mathrm{~A}$ | $\mathrm{V}_{\mathrm{CC}}-0.5$ | - | $\mathrm{V}_{\text {c }}$ | V |
| $\mathrm{V}_{\text {OL(DAT) }}$ | LOW-level data output voltage | $\mathrm{I}_{\text {DATA }}=200 \mu \mathrm{~A}$ | 0 | - | 0.6 | V |
| RSSI comparator |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{OH} \text { (RSSI) }}$ | HIGH-level comparator output voltage | $\mathrm{I}_{\text {RSSI }}=-10 \mu \mathrm{~A}$ | $\mathrm{V}_{\mathrm{CC}}-0.5$ | - | $\mathrm{V}_{\mathrm{CC}}$ | V |
| $\mathrm{V}_{\text {OL(RSSI) }}$ | LOW-level comparator output voltage | $\mathrm{I}_{\mathrm{RSSI}}=200 \mu \mathrm{~A}$ | 0 | - | 0.6 | V |

## Notes

1. The given values are valid for the whole temperature range from $\mathrm{T}_{\mathrm{amb}}=-40$ to $+85^{\circ} \mathrm{C}$.
2. Tune RF input frequency until IF $=1 \mathrm{MHz}$.

## AC CHARACTERISTICS

$\mathrm{V}_{\mathrm{CC}}=3.5 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; for application diagram see Fig. 11 ; $\mathrm{f}_{\mathrm{i}}=433.92 \mathrm{MHz} ; \Delta \mathrm{f}= \pm 25 \mathrm{kHz} ; \mathrm{f}_{\mathrm{mod}}=250 \mathrm{~Hz}$ square wave, i.e. $500 \mathrm{bits} / \mathrm{s}$; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| System performance |  |  |  |  |  |  |
| $\mathrm{P}_{\text {sens }}$ | sensitivity | BER $\leq 3 \%$ | - | - | -94 | dBm |
| $\mathrm{P}_{\mathrm{i}(\text { max })}$ | maximum input power | BER $\leq 3 \%$ | - | - | -30 | dBm |
| $\alpha_{\text {rad }}$ | spurious radiation | note 1 | - | - | -60 | dBm |
| $\mathrm{t}_{\text {st }}$ | receiver settling time | $\mathrm{P}_{\mathrm{i}}=\mathrm{P}_{\text {sens }}+10 \mathrm{~dB}$; see Fig. 5 | - | 2 | 5 | ms |
| $\mathrm{B}_{\text {IF }}$ | IF bandwidth range | $\mathrm{P}_{\mathrm{i}}=\mathrm{P}_{\text {sens }}+3 \mathrm{~dB}$ | 850 | 1000 | 1150 | kHz |
| $\mathrm{f}_{\mathrm{D}}$ | data frequency |  | 140 | - | 250 | Hz |
| Mixer |  |  |  |  |  |  |
| $\mathrm{G}_{\text {mix }}$ | mixer conversion gain |  | 31 | 33 | 35 | dB |
| $\mathrm{R}_{0 \text { (mix) }}$ | mixer output resistance |  | 2.7 | 3 | 3.3 | $\mathrm{k} \Omega$ |

## Post mixer amplifier

| IP3 PMA | interception point (mixer + PMA) | note 2 | -38 | -35 | - | dBm |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{G}_{\text {PMA }}$ | PMA gain | note 2 | 9 | 10.4 | 12 | dB |
| $\mathrm{P}_{<1 \mathrm{~dB}}$ | compression (mixer + PMA) | $\mathrm{P}_{\mathrm{i}}=-45 \mathrm{dBm}$ | 0 | - | 1 | dBm |
| BW PMA | PMA LP cut-off frequency |  | 5 | - | - | MHz |
| $\mathrm{R}_{\text {oPMA }}$ | PMA output resistance |  | 1.2 | 1.4 | 1.6 | $\mathrm{k} \Omega$ |


| Limiter |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| $\mathrm{G}_{\lim }$ | limiter gain |  | 60 | 63.5 | 67 | dB |  |
| $\mathrm{~B}_{\lim }$ | limiter LP cut-off frequency |  | 2 | 5 | 8 | MHz |  |
| $\mathrm{R}_{\mathrm{i}(\text { lim })}$ | limiter input resistance |  | 40 | 50 | 60 | $\mathrm{k} \Omega$ |  |


| Demodulator |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GDMOD | demodulator gain | note 2 | 0.8 | 1 | 1.2 | $\frac{\mathrm{mV}}{\mathrm{kHz}}$ |
| $\mathrm{f}_{\text {( }{ }^{\text {(DMOD }} \text { ) }}$ | demodulator centre frequency |  | 800 | 1000 | 1200 | kHz |
| $\Delta \mathrm{f}$ | frequency deviation |  | 20 | 25 | 70 | kHz |
| $\mathrm{R}_{0 \text { (DMOD) }}$ | demodulator output resistance |  | 24 | 30 | 36 | $\mathrm{k} \Omega$ |
| Data slicer |  |  |  |  |  |  |
| $\mathrm{B}_{\mathrm{DS}}$ | data slicer bandwidth |  | 35 | 50 | - | kHz |
| $\mathrm{R}_{0 \text { (DS) }}$ | data slicer output resistance |  | 120 | 150 | 180 | k $\Omega$ |


| RSSI comparator |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{0 \text { (RSSI) }}$ | RSSI output voltage | see Fig. 3 | - | - | - | - |
| $\mathrm{V}_{\text {O(COMP) }}$ | COMP output voltage | see Fig. 4 | - | - | - | - |
| $\mathrm{P}_{\mathrm{th} \text { (on) }}$ | threshold for switching COMP output voltage to HIGH |  | -99.5 | -95.5 | -91.5 | dBm |
| $\mathrm{P}_{\text {hys( }}$ W) | hysteresis width of COMP output voltage |  | 1 | 2 | 4 | dBm |

## Notes

1. Measured at the RF input connector of the test board.
2. Measured at test point $A$ in Fig. 11.

(1) $\mathrm{T}_{\mathrm{amb}}=85^{\circ} \mathrm{C}$.
(2) $\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$.
(3) $\mathrm{T}_{\mathrm{amb}}=-40^{\circ} \mathrm{C}$.

Fig. 3 RSSI output voltage as a function of RF input power.


Fig. 4 Comparator output voltage as a function of HF input power.

Frequency Shift Keying (FSK) receiver

## INTERNAL CIRCUITRY

Table 1 Equivalent pin circuits and pin voltages for rough test of printed circuit board; $\mathrm{V}_{\mathrm{CC}}=3.5 \mathrm{~V}$; no input signal

| PIN | SYMBOL | DC VOLTAGE <br> (V) | EQUIVALENT CIRCUIT |
| :---: | :---: | :---: | :---: |
| 1 | MON | 2.98 |  |
| 2 | MOP | 2.98 |  |
| 3 | $\mathrm{V}_{\text {cc }}$ | - |  |
| 4 | OSC | 3.34 |  |
| 5 | OSE | - |  |
| 6 | $\mathrm{V}_{\mathrm{EO}}$ | 0 |  |
| 7 | $\mathrm{V}_{\mathrm{EE}}$ | 0 |  |
| 8 | COMP | - |  |
| 9 | CPB | 1.93 |  |
| 10 | CPA | 1.93 |  |

Frequency Shift Keying (FSK) receiver

| PIN | SYMBOL | DC VOLTAGE <br> (V) | EQUIVALENT CIRCUIT |
| :---: | :---: | :---: | :---: |
| 11 | DATA | - |  |
| 12 | PWD | - |  |
| 13 | CPC | 1.93 |  |
| 14 | DMOD | 1.83 |  |

Frequency Shift Keying (FSK) receiver

| PIN | SYMBOL | DC VOLTAGE <br> (V) | EQUIVALENT CIRCUIT |
| :---: | :---: | :---: | :---: |
| 15 | RSSI | 2.36 |  |
| 16 | LFB | 2.81 |  |
| 17 | LIN | 3.49 |  |

Frequency Shift Keying (FSK) receiver

| PIN | SYMBOL | DC VOLTAGE <br> (V) | EQUIVALENT CIRCUIT |  |
| :--- | :--- | :---: | :---: | :---: |
| 18 | MXIN | 0.78 |  |  |
| 19 | $\mathrm{~V}_{\mathrm{EM}}$ | 0 |  |  |
| 20 | FA | 2.27 |  |  |

## TEST INFORMATION

## Tuning procedure for AC tests

1. Turn on the signal generator ( $\mathrm{f}_{\mathrm{i}}=433.92 \mathrm{MHz}$; no modulation; $R F$ input level $=-60 \mathrm{dBm}$ ).
2. Tune C 6 (RF stage input) to obtain a peak voltage on test point $A$ (see Fig.11).
3. Turn on modulation ( $\mathrm{f}_{\mathrm{i}}=433.92 \mathrm{MHz} ; \mathrm{f}_{\mathrm{mod}}=250 \mathrm{~Hz}$ square wave; $\Delta \mathrm{f}=25 \mathrm{kHz} ; \mathrm{RF}$ input level $=-60 \mathrm{dBm}$ ).
4. Check that data is appearing on the data output (pin 11) and proceed with the AC tests.

## AC test conditions

Table 2 Test signals
The reference signal level $P_{\text {ref }}$ for the following tests is defined as the minimum input level in dBm to give a BER $\leq 3 \times 10^{-2}$ (e.g. 15 bit errors per second for 500 bits/s).

| TEST <br> SIGNAL | FREQUENCY <br> $(\mathbf{M H z})$ | DATA SIGNAL | MODULATION | FREQUENCY <br> DEVIATION |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 433.92 | 250 Hz square wave | FM (FSK) | 25 kHz |
| 2 | 433.92 | - | no modulation | - |
| 3 | 433.82 | - | no modulation | - |

Table 3 Test results
$P_{1}$ is the maximum available power from signal generator 1 at the input of the test board; $P_{2}$ is the maximum available power from signal generator 2 at the input of the test board.

| TEST | GENERATOR |  | RESULT |
| :---: | :---: | :---: | :---: |
|  | 1 | 2 |  |
| Sensitivity into pin MXIN (see Fig.6) | modulated test signal $1 ; \mathrm{P}_{1} \leq-94 \mathrm{dBm}$ | - | $\mathrm{BER} \leq 3 \times 10^{-2}$ <br> (e.g. 15 bit errors per second for 500 bits/s) |
| Maximum input power (see Fig.6) | modulated test signal $1 ; P_{1} \geq-30 d B m$ (minimum $\mathrm{P}_{\max }$ ) | - | $\begin{aligned} & \text { BER } \leq 3 \times 10^{-2} \\ & \text { (e.g. } 15 \text { bit errors per second for } 500 \text { bits/s) } \end{aligned}$ |
| Receiver turn-on time; note 1 | test signal 1; $P_{1}=P_{\text {ref }}+10 \mathrm{~dB}$ | - | check that the first 10 bits are correct; error counting is started 10 ms after PWD switched to operating mode: ON |
| Intercept point (mixer + PMA) see note 2 and Fig. 7 | test signal 3; $P_{1}=-55 \mathrm{dBm}$ | test signal 2; $P_{2}=P_{1}$ | $\mathrm{IP} 3=\mathrm{P}_{1}+1 / 2 \times \mathrm{IM} 3$ (dB); IP3 $\geq-38 \mathrm{dBm}$ |
| Spurious radiation see note 3 and Fig. 8 | - | - | no spurious radiation ( $25 \mathrm{MHz}-1 \mathrm{GHz}$ ) with level higher than -60 dBm (maximum $\mathrm{P}_{\text {spur }}$ ) |
| 1 dB compression point (mixer + PMA) see note 2 and Fig. 9 | test signal 3; <br> $P_{11}=-70 \mathrm{dBm}$; <br> $\mathrm{P}_{12}=-45 \mathrm{dBm}$ <br> (minimum $\mathrm{P}_{1 \mathrm{~dB}}$ ) | - | $\left(\mathrm{P}_{\mathrm{o} 1}+70 \mathrm{~dB}\right)-\left[\mathrm{P}_{\mathrm{o} 2}+45 \mathrm{~dB}\right.$ (minimum $\left.\left.P_{1 d B}\right)\right] \leq 1 d B$, where $P_{01}, P_{o 2}$ is the output power for test signals with $P_{11}$ or $P_{12}$, respectively |

## Notes

1. The power-down voltage $\mathrm{V}_{\mathrm{PWD}}$ alternates between operating mode $\mathrm{ON}(100 \mathrm{~ms})$ and $\mathrm{OFF}(100 \mathrm{~ms})$; see Fig. 5 .
2. Probe of spectrum analyzer connected to test point $A$.
3. Spectrum analyzer connected to the input of the test board.


Fig. 5 Timing diagram for pulsed power-down voltage.

(1) For test circuit see Fig. 11.
(2) For BER test facility see Fig. 10.

Fig. 6 Test configuration A (single generator).

(1) For test circuit see Fig. 11.

Fig. 7 Test configuration B (IP3).

(1) For test circuit see Fig. 11.

Fig. 8 Test configuration C (spurious radiation).

(1) For test circuit see Fig.11.

Fig. 9 Test configuration $\mathrm{D}(1 \mathrm{~dB}$ compression point).


Fig. 10 BER test facility.

Frequency Shift Keying (FSK) receiver

## APPLICATION INFORMATION


(1) Stray inductance.

Table 4 Application component list for Fig. 11

| COMPONENT | VALUE | TOLERANCE | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| R2 | $560 \Omega$ | $\pm 2 \%$ | TC = $50 \mathrm{ppm} / \mathrm{K}$ |
| R3 | $220 \Omega$ | $\pm 2 \%$ | TC = $50 \mathrm{ppm} / \mathrm{K}$ |
| R4 | $820 \mathrm{k} \Omega$ | $\pm 2 \%$ | TC = $50 \mathrm{ppm} / \mathrm{K}$ |
| C1 | $4.7 \mu \mathrm{~F}$ | $\pm 20 \%$ | - |
| C2 | 150 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C3 | 100 nF | $\pm 10 \%$ | $\mathrm{TC}=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C4 | 100 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C5 | 2.7 pF | $\pm 10 \%$ | TC $=0 \pm 150 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 30 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C6 | 3 to 10 pF | - | TC $=0 \pm 300 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 20 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C7 | 56 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C8 | 33 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C9 | 100 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C10 | 5.6 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 20 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C11 | 100 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C12 | 100 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| C13 | 2.2 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| C14 | 33 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| C16 | 3.9 pF | $\pm 10 \%$ | TC $=0 \pm 150 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 30 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C17 | 10 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| C18 | 1.8 pF | $\pm 10 \%$ | TC $=0 \pm 150 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 30 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C19 | 39 pF | $\pm 10 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C20 | 3.3 pF | $\pm 10 \%$ | TC $=0 \pm 150 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 30 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C22 | 18 pF | $\pm 5 \%$ | TC $=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C23 | 47 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| C24 | 22 pF | $\pm 5 \%$ | $\mathrm{TC}=0 \pm 30 \mathrm{ppm} / \mathrm{K} ; \tan \delta \leq 10 \times 10^{-4} ; \mathrm{f}=1 \mathrm{MHz}$ |
| C25 | 1 nF | $\pm 10 \%$ | $\tan \delta \leq 25 \times 10^{-3} ; \mathrm{f}=1 \mathrm{kHz}$ |
| L1 | 10 nH | $\pm 10 \%$ | $\mathrm{Q}_{\text {min }}=50$ to 450 MHz ; TC = 25 to $125 \mathrm{ppm} / \mathrm{K}$ |
| L2 | $150 \mu \mathrm{H}$ | $\pm 10 \%$ | $\mathrm{Q}_{\text {min }}=45$ to $800 \mathrm{kHz} ; \mathrm{C}_{\text {stray }} \leq 1 \mathrm{pF}$ |
| L3 | $220 \mu \mathrm{H}$ | $\pm 10 \%$ | $\mathrm{Q}_{\text {min }}=45$ to $800 \mathrm{kHz} ; \mathrm{C}_{\text {stray }} \leq 1 \mathrm{pF}$ |
| L4 | 33 nH | $\pm 10 \%$ | $\mathrm{Q}_{\text {min }}=45$ to 450 MHz ; TC = 25 to $125 \mathrm{ppm} / \mathrm{K}$ |
| L5 | $470 \mu \mathrm{H}$ | $\pm 10 \%$ | $\mathrm{Q}_{\text {min }}=45$ to $800 \mathrm{kHz} ; \mathrm{C}_{\text {stray }} \leq 1 \mathrm{pF}$ |

Table 5 Surface Acoustic Wave Resonator (SAWR) data

| DESCRIPTION | SPECIFICATION |
| :--- | :--- |
| Type | one-port |
| Centre frequency | $432.92 \mathrm{MHz} \pm 75 \mathrm{kHz}$ |
| Maximum insertion loss | 1.5 dB |
| Typical loaded Q | $1600(50 \Omega$ load $)$ |
| Temperature drift | $0.032 \mathrm{ppm} / \mathrm{K}^{2}$ |
| Turnover temperature | $43^{\circ} \mathrm{C}$ |

## LAYOUT OF PRINTED-CIRCUIT BOARD FOR AC APPLICATION


a. Copper side.

b. Component side.

Fig. 12 Printed-circuit board layout.

## PACKAGE OUTLINE

SSOP20: plastic shrink small outline package; 20 leads; body width 5.3 mm
SOT339-1


DIMENSIONS (mm are the original dimensions)

| UNIT | A max. | $\mathrm{A}_{1}$ | $\mathrm{A}_{2}$ | $\mathrm{A}_{3}$ | $\mathrm{b}_{\mathrm{p}}$ | c | $D^{(1)}$ | $E^{(1)}$ | e | $\mathrm{H}_{\mathrm{E}}$ | L | $L_{p}$ | Q | v | w | y | $Z^{(1)}$ | $\theta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 2.0 | $\begin{aligned} & 0.21 \\ & 0.05 \end{aligned}$ | $\begin{aligned} & 1.80 \\ & 1.65 \end{aligned}$ | 0.25 | $\begin{aligned} & 0.38 \\ & 0.25 \end{aligned}$ | $\begin{aligned} & 0.20 \\ & 0.09 \end{aligned}$ | $\begin{aligned} & 7.4 \\ & 7.0 \end{aligned}$ | $\begin{aligned} & \hline 5.4 \\ & 5.2 \end{aligned}$ | 0.65 | $\begin{aligned} & 7.9 \\ & 7.6 \end{aligned}$ | 1.25 | $\begin{aligned} & 1.03 \\ & 0.63 \end{aligned}$ | $\begin{aligned} & 0.9 \\ & 0.7 \end{aligned}$ | 0.2 | 0.13 | 0.1 | $\begin{aligned} & 0.9 \\ & 0.5 \end{aligned}$ | $8^{\circ}$ 0 |

Note

1. Plastic or metal protrusions of 0.20 mm maximum per side are not included.

| OUTLINE VERSION | REFERENCES |  |  | EUROPEAN PROJECTION | ISSUE DATE |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | IEC | JEDEC | EIAJ |  |  |
| SOT339-1 |  | MO-150AE |  | $\square \oplus$ | $\begin{aligned} & 93-09-08 \\ & 95-02-04 \end{aligned}$ |

## SOLDERING

## Introduction

There is no soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and surface mounted components are mixed on one printed-circuit board. However, wave soldering is not always suitable for surface mounted ICs, or for printed-circuits with high population densities. In these situations reflow soldering is often used.

This text gives a very brief insight to a complex technology. A more in-depth account of soldering ICs can be found in our "IC Package Databook" (order code 9398652 90011).

## Reflow soldering

Reflow soldering techniques are suitable for all SSOP packages.

Reflow soldering requires solder paste (a suspension of fine solder particles, flux and binding agent) to be applied to the printed-circuit board by screen printing, stencilling or pressure-syringe dispensing before package placement.

Several techniques exist for reflowing; for example, thermal conduction by heated belt. Dwell times vary between 50 and 300 seconds depending on heating method. Typical reflow temperatures range from 215 to $250^{\circ} \mathrm{C}$.

Preheating is necessary to dry the paste and evaporate the binding agent. Preheating duration: 45 minutes at $45^{\circ} \mathrm{C}$.

## Wave soldering

Wave soldering is not recommended for SSOP packages. This is because of the likelihood of solder bridging due to closely-spaced leads and the possibility of incomplete solder penetration in multi-lead devices.

If wave soldering cannot be avoided, the following conditions must be observed:

- A double-wave (a turbulent wave with high upward pressure followed by a smooth laminar wave) soldering technique should be used.
- The longitudinal axis of the package footprint must be parallel to the solder flow and must incorporate solder thieves at the downstream end.

Even with these conditions, only consider wave soldering SSOP packages that have a body width of 4.4 mm , that is SSOP16 (SOT369-1) or SSOP20 (SOT266-1).

During placement and before soldering, the package must be fixed with a droplet of adhesive. The adhesive can be applied by screen printing, pin transfer or syringe dispensing. The package can be soldered after the adhesive is cured.

Maximum permissible solder temperature is $260^{\circ} \mathrm{C}$, and maximum duration of package immersion in solder is 10 seconds, if cooled to less than $150^{\circ} \mathrm{C}$ within 6 seconds. Typical dwell time is 4 seconds at $250^{\circ} \mathrm{C}$.

A mildly-activated flux will eliminate the need for removal of corrosive residues in most applications.

## Repairing soldered joints

Fix the component by first soldering two diagonallyopposite end leads. Use only a low voltage soldering iron (less than 24 V ) applied to the flat part of the lead. Contact time must be limited to 10 seconds at up to $300^{\circ} \mathrm{C}$. When using a dedicated tool, all other leads can be soldered in one operation within 2 to 5 seconds between 270 and $320^{\circ} \mathrm{C}$.

## DEFINITIONS

| Data sheet status |  |
| :--- | :--- |
| Objective specification | This data sheet contains target or goal specifications for product development. |
| Preliminary specification | This data sheet contains preliminary data; supplementary data may be published later. |
| Product specification | This data sheet contains final product specifications. |
| Limiting values |  |
| Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 134). Stress above one or <br> more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation <br> of the device at these or at any other conditions above those given in the Characteristics sections of the specification <br> is not implied. Exposure to limiting values for extended periods may affect device reliability. |  |
| Application information |  |
| Where application information is given, it is advisory and does not form part of the specification. |  |

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